# High resolution topography of Titan adapting the Delay-Doppler algorithm to the Cassini RADAR Altimeter Data 

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#### Abstract

The Cassini RADAR altimeter has provided broadscale surface topography data for Saturn's largest moon Titan. Herein, we adapt the Delay-Doppler algorithm to take into account Cassini geometries and antenna mispointing usually occurring during hyperbolic Titan flybys. The proposed algorithm allows up to tenfold improvement in the along-track resolution. Preliminary results are provided that show how the improved topography presented herein can advance our understanding of Titan's surface characteristics.


Index Terms-Radar, Spaceborne Radar, Radar Altimetry, Radar Signal Processing, Delay/Doppler Algorithm, Planetary Science, Cassini, Titan.

## I. Introduction

TThe Cassini RADAR is a multimode Ku-band (13.78 GHz) radar instrument [1] that provided topographic information of the surface of Saturn's largest moon, Titan, from 2004 to 2017 (see Table 1, instrument parameters). During the course of its mission, the Cassini spacecraft performed a total of 127 flybys of Titan, activating the altimetric mode [ $2 ; 3 ; 4$ ] during 40 of them (see Table 1, zonal distribution). In Table 2 we report the whole Cassini dataset of altimetric acquisitions with the best ground resolution achieved in along track during each flyby and the most important surface features [5] observed from Cassini Synthetic aperture radar (SAR) mapping. SAR mode, indeed, has been able to provide imaging at $\leq 300 \mathrm{~m} /$ pixel of $\sim 20 \%$ of the surface $(\sim 50 \%$ at $\leq 1500 \mathrm{~m} /$ pixel). Other modes of the radar, not dealt with in this paper, enabled the measurement of microwave thermal

[^0]

Fig. 1. Delay/Doppler altimetry: geometry of acquisition. (a) Conventional radar altimetry estimates the distance between radar and underlying surface by averaging all the echoes returning from the footprint. (b) Delay/Doppler altimetry exploits Doppler selectivity to discriminate echoes returning from different cells along-track, thus enabling an extra dimension in the measurement space.
energy emitted by the surface (radiometry) and the acquisition of low-resolution backscatter images (scatterometry).

The specific geometry of Cassini acquisitions (hyperbolic), caused the range of spacecraft altitudes to span up to several thousand kilometers along a single altimetric track. This wide range of altitudes caused in turn the ground resolution to significantly vary during each flyby.

Doppler processing techniques have been demonstrated to greatly improve the performances of conventional radar altimeters for terrestrial applications as well as planetary purposes. For example, Doppler beam sharpening is a well-known powerful technique that greatly increases the along-track resolution of altimetric data [6;7].

Doppler-resolved altimetry processing allows non-coherent integration of the overlapped Doppler bins (see Fig. 1) by compensating time delay offsets due to the different paths travelled by signals to reach the same frequency-resolved surface footprints. This technique was originally applied to radar data from the Magellan mission to Venus, revealing much more details of the surface [6] and obtaining up to a seven times enhancement of the along-track resolution.

Based on the same principle, [8] introduced the DelayDoppler algorithm (DDA) used today in terrestrial radar applications, such as the Cryosat-2, AltiKa, and Sentinel-3 missions
(e.g., $[9 ; 10]$ ). The DDA is also crucial to ESA's COASTAL and SAMOSA projects for coastal monitoring, where the increased spatial resolution is allowing the recovery of large quantities of otherwise discarded data acquired near coastlines and on inland waters [11].

This paper describes how to implement the delay/Doppler algorithm to the specific case of the Cassini radar altimeter data. The algorithm is adapted to take into account the hyperbolic geometry of Cassini spacecraft and the antenna mispointing $\left(\theta_{\text {off }}\right)$ that usually occurs during Titan flybys (see Table 1, antenna mispointing).

| TABLE I |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RADAR INSTRUMENT PARAMETERS |  |  |  |  |
| Wavelength $(\lambda)=2.17 \mathrm{~cm}$ |  |  |  |  |
| Chirped signal duration $(\tau)=150 \mu \mathrm{~s}$ |  |  |  |  |
| Chirped signal bandwidth (B) $=4.25 \mathrm{MHz}$ |  |  |  |  |
| Burst repetition interval (BRI) $=0.5 / 4 \mathrm{~s}$ |  |  |  |  |
| Number of pulses within each burst $\left(N_{R X}\right)=15$ |  |  |  |  |
| Pulse repetition frequency (PRF) $=5 \mathrm{kHz}$ |  |  |  |  |
| Peak transmitted power $\left(P_{T X}\right)=40.084 \mathrm{~W}$ |  |  |  |  |
| Antenna -3dB beamwidth $\left(\theta_{3 d B}\right)=6.1 \mathrm{mrad}$ |  |  |  |  |
| Peak antenna gain $\left(G_{0}\right)=50.7 \mathrm{~dB}$ |  |  |  |  |
| Spacecraft altitude in altimetry mode $(\mathrm{H})=1000$ to 9000 km |  |  |  |  |
| Spacecraft tangential velocity $\left(\mathrm{v}_{\mathrm{t}}\right)=2 / 6 \mathrm{~km} / \mathrm{s}$ |  |  |  |  |
| Spacecraft radial velocity ( $v_{\text {rad }}$ ) $=0 / 5.2 \mathrm{~km} / \mathrm{s}$ |  |  |  |  |
| ZONAL DISTRIBUTION ( $\pm 45^{\circ} \mathrm{BORDERS}$ ) |  |  |  |  |
| Area of Titan | North | Equator | South |  |
| Dataset \% | 17 | 78 | 5 |  |
| ANTENNA MISPOINTING |  |  |  |  |
| $\theta_{\text {off }}\left({ }^{\circ}\right.$ ) | $\theta<0.01$ | $0.01<\theta<0.04$ | $0.04<\theta<0.2$ | $\theta>0.2$ |
| Dataset \% | 29 | 28 | 40 | 3 |

An interested reader could also refer to [4] for a non-coherent model of the average impulse response of a rough surface that has been developed for the Cassini radar altimeter.

## II. Delay/Doppler Processing adapted to Cassini RADAR ALTIMETER DATA

The along-track resolution achievable by a delay-Doppler algorithm [8] is given by

$$
\begin{equation*}
\delta \mathrm{d}=\frac{\mathrm{H} \cdot \lambda \cdot \mathrm{PRF}}{2 \cdot \mathrm{v}_{\mathrm{t}} \cdot N} \tag{1}
\end{equation*}
$$

with $H$ the spacecraft altitude, $\lambda$ the transmitted signal wavelength, $\mathrm{v}_{\mathrm{t}}$ the spacecraft tangential velocity and N is the number of Doppler filters useful for the processing, that can be expressed by:

$$
\begin{equation*}
N=\frac{B_{D}}{\delta f} \tag{2}
\end{equation*}
$$

with $B_{D}=2 \mathrm{v}_{\mathrm{t}} \sin (\varphi) / \lambda$ the Doppler bandwidth, $\delta f=$ PRF/ $N_{R X}$ the Doppler resolution, $N_{R X}$ the total number of echoes received within the burst (or the number of available filters), $\varphi$ an integration angle depending on spacecraft altitude and encompassing the antenna aperture from which echo power is received (see appendix of [6] for more details).

Figure 2 shows the complete block diagram of the DDA applied to the Cassini radar altimeter data. The main steps of the proposed processing are:

TABLE II
ALTIMETRY DATASET (TA-T126) AND SURFACE UNITS OBSERVED

| Swath Name | Day | Number of Alt. Bursts | Min. <br> Real- <br> Aperture <br> Footprint <br> [km] | Landforms in Track |
| :---: | :---: | :---: | :---: | :---: |
| Ta | 26/10/2004 | 458 | 31 | HM; CR; |
| T3 | 15/02/2005 | 291 | 36 | HM; DU; |
| T8 | 28/10/2005 | 742 | 31 | DU; HM; |
| T13 | 30/04/2006 | 268 | 34 | DU; |
| T16 | 21/07/2006 | 886 | 32 | HM; DU; |
| T19 | 9/10/2006 | 911 | 31 | BP; |
| T20 | 25/10/2006 | 20 | 81 | BP |
| T21 | 12/12/2006 | 444 | 35 | DU; |
| T23 | 13/01/2007 | 887 | 31 | BP; PL; |
| T25 | 22/02/2007 | 57 | 32 | HM; |
| T28 | 10/4/2007 | 1248 | 33 | PL; HM; |
| T29 | 26/04/2007 | 982 | 33 | HM; PLS; |
| T30 | 12/5/2007 | 3439 | 6 | HM; DU; PL; EL; MO; |
| T36 | 2/10/2007 | 1833 | 34 | HM; DU; PL; |
| T39 | 20/12/2007 | 633 | 34 | HM; DU; PL; |
| T41 | 22/02/2008 | 398 | 7 | HM; MO; PLS; |
| T43 | 12/5/2008 | 590 | 35 | PL; |
| T44 | 28/05/2008 | 654 | 30 | BP; MO; |
| T48 | 5/12/2008 | 130 | 33 | NCBS; |
| T49 | 21/12/2008 | 912 | 8 | MO; FL; RI; |
| T50 | 7/2/2009 | 404 | 28 | HM; PL; |
| T55 | 21/05/2009 | 637 | 33 | BP; |
| T56 | 6/6/2009 | 261 | 32 | HM; PL; BP; |
| T57 | 22/06/2009 | 562 | 26 | NCBS; PLS; |
| T61 | 25/08/2009 | 133 | 31 | DU; |
| T64 | 27/12/2009 | 586 | 30 | HM; DU; |
| T77 | 20/06/2011 | 1688 | 8 | DU; PL; BP; |
| T83 | 21/05/2012 | 626 | 30 | HM; CR; DU; BP; |
| T84 | 6/6/2012 | 626 | 31 | BP; |
| T86 | 26/09/2012 | 61 | 38 | HM; BP; |
| T91 | 23/05/2013 | 1335 | 6 | DU; BP; EL; FL; RI; |
| T92 | 10/7/2013 | 280 | 31 | FL; |
| T95 | 14/10/2013 | 212 | 31 | FL; |
| T98 | 2/2/2014 | 2236 | 8 | HM; DU; BP; MO; PLS; |
| T104 | 21/08/2014 | 645 | 10 | FL; |
| T108 | 11/1/2015 | 456 | 6 | HM; DU; BP; EL; FL; RI; |
| T113 | 28/09/2015 | 204 | 31 | DU; BP; |
| T120 | 7/6/2016 | 290 | 30 | DU; BP; |
| T121 | 25/7/2016 | 292 | 30 | CR; |
| T126 | 22/4/2017 | 472 | 7 | PL; EL; FL; |

HM: inselbergs/hummocks; CR: craters; DU: dunes; BP: bright planes; PL: planes; EL: empty lakes; FL: filled lakes; RI: rivers; MO: mountains; PLS: possible liquid surface; NCBS: not covered by SAR.
a) extraction of ancillary data and range compression executed during conventional processing of the altimetric data (for a detailed description please see [3; 12; 13]);
b) phase shift compensation due to the radial velocity variations experienced by the spacecraft during its hyperbolic Titan flybys and to the antenna mispointing;
c) along-track Discrete Fourier Transform (DFT) is performed to pass into the range - Doppler domain. Weighting windows are applied here to mitigate sidelobes;
d) (optional step) application of a super-resolution technique in range (i.e., see [14]);
e) range-delay compensation taking into account the spacecraft attitude (i.e. off-nadir angle);
f) antenna gain pattern compensation;
g) incoherent average of Doppler cells;
h) altimetry profiles generation.

After the extraction of ancillary data and range compression (step a), we compensate the phase shift caused by the spacecraft radial velocity (step b) by multiplying the Cassini burst for:

$$
\begin{equation*}
\Omega\left(\mathrm{t}^{\prime}\right)=\exp \left\{-j \frac{4 \pi \cdot v_{r a d} \cdot t^{\prime}}{\lambda}\right\} \tag{3}
\end{equation*}
$$

with $v_{r a d}$ the spacecraft radial velocity and $t^{\prime}$ is the slowtime, indicated as a discrete intra-burst time vector defined as $\mathrm{n} / \mathrm{PRF}$, with $n=1: N_{R X}$.

The 4.25 MHz chirp bandwidth of the Cassini RADAR altimeter allows production of relative elevation profiles with a vertical resolution of 35 m . However, studies performed by [14] concerning the application of parametric autoregressive (AR) time-series models revealed the possibility to improve the range resolution of the radar by a factor of up to $x 3$. This method has been successfully adopted by Mastrogiuseppe et al. [15, 16, 17] on Cassini, and by Raguso et al. [18; 19] on SHARAD and MARSIS data. These works demonstrated that the application of parametric AR time-series models (i.e., Burg's Maximum Entropy Method) can effectively be used to improve range resolution of coherent radar returns with the advantage that the linearity of this kind of processes makes recompressed pulses still suitable for backscattering and phase responses studies [14]. The discretionary implementation of this step of processing (step d) can include the application of any super-resolution technique in range just after performing the DFT in along-track (step c).

The key-step of the delay-Doppler processing is the compensation of the range-delay associated to all the filters of the azimuthal Fourier transform and relative to different alongtrack positions (step e). The goal of this operation is to allow signals to have the same range when the successive step of incoherent integration will be executed.
In frequency domain these delays correspond to constant (CW) frequency shifts that can be compensated by multiplying the signal content at each Doppler position $\left(f^{\prime}\right)$ by an equal and opposite range CW signal [8]:

$$
\begin{equation*}
\Phi\left(f^{\prime}, t\right)=\exp \left\{+j \frac{4 \pi \cdot k \cdot \delta r\left(f^{\prime}\right) \cdot t}{c}\right\} \tag{4}
\end{equation*}
$$

with

$$
\begin{equation*}
\delta r\left(f^{\prime}\right) \cong \alpha_{R} \frac{\lambda^{2} f^{\prime 2} H}{8 v_{t}^{2}} \tag{5}
\end{equation*}
$$

where k is the chirp rate, c is the speed of light and $\alpha_{R} \cong$ $R_{T} /\left(R_{T}+H\right)$ is Titan's surface curvature [4], and t the fasttime. In this context, the frequency in range is proportional to the delay respect to the altimeter tracking-point and the frequency in along-track is indicative of relative position of a scatterer respect to the zero-Doppler point. In our work, the formula (5) is calculated according to the antenna mispointing angle of the observation (along track component or pitch angle), which is recorded into the Cassini SPICE kernels. Antenna mispointing causes an additional increment of delay due to


Fig. 2. Delay/Doppler processing work-flow adapted for the Cassini mission.
the Doppler frequency shift introduced. While this Doppler shift is compensated in step $b$, the delay increments are calculated taking into account the actual Doppler frequency $\left(f^{\prime}\right)$ of each bin at the time of observation. The additional increment of frequency $\left(f_{D}\right)$ is calculated from off-nadir and is added to the Doppler frequency calculated at nadir $(f)$ :

$$
\begin{equation*}
f^{\prime}=f-f_{D} \tag{6}
\end{equation*}
$$

with

$$
\begin{equation*}
f_{D}=\frac{2 \cdot v_{t} \cdot \sin \theta_{\text {off }}}{\lambda} \tag{7}
\end{equation*}
$$

The compensation of antenna gain pattern is performed (step f) by considering a gaussian antenna beam:

$$
\begin{equation*}
G(f) \approx G_{0} \exp \left\{-\frac{1}{2 \gamma}\left(\frac{\lambda \cdot f}{v_{t}}\right)^{2}\right\} \tag{8}
\end{equation*}
$$

with

$$
\begin{equation*}
\gamma=-\frac{2 \sin ^{2}\left(\theta_{3 d B} / 2\right)}{\ln 0.5} \tag{9}
\end{equation*}
$$

Note that the gain pattern compensation is accomplished by applying a signal adaptive 2-D mask able to compensate the gain effects when signal is present. Specifically, the noise is evaluated and only signal having a Signal-to-Noise Ratio (SNR) $>10 \mathrm{~dB}$ is compensated for gain. This allows to avoid gain compensation of noise pixels, similarly to what is done for the Cassini SAR images processing [20].
Finally, we sort the individual Doppler components from subsequent, but different, bursts in order to perform their incoherent average (step g). This operation is performed by locating the Doppler cells on the (spherical) surface of Titan and calculating their relative orthodromic distance by means of the geographical information contained in the Cassini SPICE kernels. At this point, a high resolution radargram is generated (step h).


Fig. 3. (top) Delay/Doppler vs Standard processing: SNR obtained with BRI = 0.5 s and $\sigma^{0}=0 \mathrm{~dB}$; (middle) Improvement in along-track resolution given by the delay-Doppler (black solid line) in comparison with the standard processing (red solid line); with a black dashed line is indicated the number of looks at each Doppler cell. Note the variation in slope at 7500 km due to the switch from beam- to pulse-limited mode; (bottom) Radiometric resolution vs Spacecraft altitude obtained with BRI $=0.5 \mathrm{~s}$ and $\sigma^{0}=0 \mathrm{~dB}$ for both the Delay-Doppler and Standard processing.

The backscattering values of DDA products is calculated inverting the radar equation:

$$
\begin{equation*}
P_{R X}=\frac{P_{T X} \mathrm{G}_{0}^{2} \lambda^{2} B \tau}{(4 \pi)^{3} H^{4}} \sigma^{0} A K N_{L} \tag{11}
\end{equation*}
$$

where $P_{R X}$ is the received power, $B \tau$ is the compression gain in range; $\sigma^{0}$ is the normalized backscattering coefficient of the terrain (dimensionless); $A$ is the area of the Doppler footprint that has a cross-track dimension equal to the diameter of the beam-/pulse-limited antenna footprint (i.e. -3 dB aperture) and an along-track dimension that can be approximated for convenience by $\delta \mathrm{d} ; N_{L}$ is the number of looks at each Doppler position (conveniently stored in a counter variable during the
processing). Note that at the beginning of any altimetric observation of the Cassini radar, a calibration routine is performed by pointing the antenna to the cold sky and relating the measured noise power to its theoretical thermal noise equivalent. The calibration is needed to determine an analog-todigital conversion parameter between the value of digitized watts, at the output of the radar receiver, and true watts. In our formula, $K=\mathrm{C} / \mathrm{L}$ accounts for this calibration parameter C and the flyby receiver attenuator value $L$, the latter adopted to keep the echo amplitude on-scale and avoid saturation [21];

The middle panel of Figure 3 shows the significative improvement in along-track resolution given by the DDA (black solid line) in comparison with the along-track resolution achieved by the conventional altimetric processing (red solid line), for spacecraft altitudes varying from 1000 to 10000 km . For example, in the case of nominal altitudes $1000-9000 \mathrm{~km}$, the DDA increases the resolution by a factor ranging from 10 to 3 with respect to the conventional processing.
The top panel of Figure 3 shows the comparison between values of SNR obtained applying the DDA (black line) and the standard processing (red line). A slight improvement in SNR and in radiometric resolution (Fig. 3, bottom panel) are observed only at the higher altitudes, where a larger number of looks is available (black dashed line, middle panel of Fig. 3) with respect to the standard processing $\left(N_{R X}=15\right)$.

The high values of SNR obtained at nominal altitudes by both the processings cause the precision in height estimation to be not significantly affected: i.e., when observing surfaces with 20 m height standard deviation, the precision in range is always better than 8 m .

## III. Results

A detailed knowledge of Titan's surface topography is currently lacking. Available topographic data (DTMs and SARTopo) have a vertical resolution of $\sim 50 \mathrm{~m}$ at best ( $\sim 150 \mathrm{~m}$ on average), with horizontal resolutions on the order of several kilometers. While this provides a coarse knowledge of the topography, it is currently not possible to resolve the key geologic features, such as dunes or fluvial valley networks, that would constrain the dominant processes that transport material across Titan's surface.

With the more effective use of the altimetry dataset that we propose, we can improve topography and knowledge of geologic features distributed across the surface of Titan, resulting in a better understanding of Titan's history and surface evolution.

Hereafter, we will provide two case studies over specific geomorphic units including hummocks and empty lake basins.
A. Hummocky terrains are SAR-bright, topographic highs that are interpreted to represent the oldest geologic terrains on Titan [5]. The SAR image in Figure 4 (panel 'e') was acquired during the Cassini T43 flyby of Titan ( $5 / 12 / 2008$ ) and shows an area in the north-eastern part of Titan's Dilmum region $\left(19.8^{\circ} \mathrm{N}, 163.7^{\circ} \mathrm{W}\right)$ which is dominated by the presence of isolated patches of higher SAR backscatter, identified as degraded hummocky terrains units within a SAR-dark undifferentiated plain. On 2/2/2014 the Cassini spacecraft executed a
new flyby of Titan (T98) during which the same hummocky region was re-observed by the radar instrument in altimetry mode from an altitude of 2600 km . The areal extent of individual hummocks was generally smaller than any given -3 dB altimetric footprint ( 16 km in diameter), but the x 7 improvement in the along-track resolution ( $\sim 2.2 \mathrm{~km}$ Doppler cell) respect to the conventional product (Figure 4, panels ' $a$ ') manifests the capability of the DDA to reveal the presence of new features (Figure 4, panels ' $b$ '), which have a direct correspondence with the radar bright features shown by SAR images (Fig. 4, panel 'e'). We applied two different height estimators over the returned echoes: Threshold and First-Moment [22]. These trackers are sensible to the most elevated portions of the surface and to the average height within the Doppler footprint respectively. The application of the threshold tracker


Fig. 4. Hummocks as seen by delay/Doppler radar altimeter. It is hard to isolate their topographic characteristics with conventional radar altimetry: their height contribute is averaged on the wider footprint scale. Thanks to a more effective use of the received power, the delay/Doppler altimetry can determine topographic characteristics of these previously unresolved features. (a) 73 bursts from T98 altimetry radargram obtained with conventional altimetry. (b) radargram obtained with Delay/Doppler altimetry processing. (c) I moment (I mom) and Threshold (Th) height estimators' altimetry profiles: solid and dotted lines respectively show results obtained for delay/Doppler and standard processing. (d) received backscatter at nadir before (black) and after delay/Doppler processing (red). (e) T43 SAR image of the region of interest with the spacecraft ground track (yellow line) and the -3 dB footprints (yellow circles), both aligned with the altimetric profiles shown in the upper panels.
spatially resolves individual hummocks and indicates the heights of these structures to be in the order of $\sim 300$ meters (Figure 4, panel 'c').
B. Empty lake basins are a geologic feature unique to Titan. Restricted to the polar regions, the lakes form closed depressions (at the coarse resolution of Cassini's SAR images) that are hundreds of meters deep and have high-sloping interior walls [23; 24]. During the flyby T28 of Titan (4/10/2007) the Cassini radar acquired a long SAR image strip ranging from the equatorial area $15^{\circ} \mathrm{S}$ to the northern seas $79^{\circ} \mathrm{N}$. In Figure 5 (panel ' $e$ ') it is shown the SAR image of the $30 \times 40 \mathrm{~km}$ empty lake basin $\left(69.5^{\circ} \mathrm{N}, 5^{\circ} \mathrm{E}\right)$ that was observed in that occasion, crossed by the flyby T30 altimetric track acquired about one month later ( $5 / 12 / 2007$ ) from an altitude of 960 km . While the diameter of the beam limited antenna footprint in this case is of $\sim 6 \mathrm{~km}$, the DDA here ensures an along track resolution of $\sim 560 \mathrm{~m}$, corresponding to a tenfold improvement. An analysis of available topographic data for Titan's lakes shows that the larger depressions have hundreds-meter high raised rims, often offset by hundreds of meters on opposite sides of the same lake [25; 24]. While conventional altimetry can only roughly describe their topography, the Doppler-resolved altimetry is


Fig. 5. An empty lake basin as seen by delay/Doppler radar altimeter. (a) 50 bursts from T30 altimetry radargram obtained with conventional altimetry. (b) radargram obtained with Delay/Doppler altimetry processing. (c) I moment (I mom) and threshold (Th) topographic profiles. (d) received backscatter at nadir before (black) and after (red) delay/Doppler processing. (e) T28 SAR image of the region with -3 dB altimetric footprints (yellow circles) and the profile's ground-track (yellow line). The perimeter of the empty lake of interest is also highlighted with a thinner yellow line.
able to produce higher resolution radargrams and height profiles (see Figure 5, panel 'a-b-c') that can be diagnostic of the process(es) responsible for sharp-edged depressions formation. In particular, the width of the raised rims and their internal/external steep slopes can be characterized now with higher precision [26].

## IV. CONCLUSION

This paper proposes a re-processing for the Cassini RADAR altimeter data for improving its along-track resolution by adapting the delay/Doppler algorithm to the Cassini geometry. This algorithm is currently widely applied for Earth observation and its application to the Cassini data provides a most detailed topography for Saturn's largest moon, Titan.

We described how to adapt the delay/Doppler algorithm to the hyperbolic orbits traveled by the Cassini spacecraft during its Titan's flybys, accounting also for the compensation of the antenna mispointing. We showed that up to a tenfold improvement in the along-track resolution is achievable with respect to the conventional processing.

Two case studies, over specific geomorphic units were presented, including hummocks and empty lake basins. These preliminary case studies demonstrated how the improvements provided by the DDA algorithm can advance our knowledge of Titan's surface and will allow for further applications over key geologic features, like equatorial dunes [27], canyons [28] or seas and lakes [29]. The processing techniques discussed herein will result in the release to the scientific community of new altimetry data products that will open a number of research fronts.

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