

Guiding of charged particle beams in curved capillary-discharge waveguides

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A new method able to transport charged particle beams along a curved path is presented. It is based on curved capillary-discharge waveguides where the induced azimuthal magnetic field is used to focus the beam and, at the same time, keep it close to the capillary axis. We show that such a solution is highly tunable, it allows to develop compact structures providing large deflecting angles and, unlike conventional solutions based on bending magnets, preserves the beam longitudinal phase space. Such a feature, in particular, is very promising when dealing with ultra-short bunches for which non-trivial manipulations on the longitudinal phase spaces are usually required when employing conventional deflecting devices. © 2018 Author(s). All article content, except where otherwise noted, is licensed under a Creative Commons Attribution (CC BY) license (http://creativecommons.org/licenses/by/4.0/). https://doi.org/10.1063/1.5011964

Nowadays there is a growing interest in the development of new compact devices able to deflect charged particle beams with large energies. In accelerator facilities dipole magnets are widely used to realize bends and translate the beam to a specific location ^{1–3} or for the generation of synchrotron radiation, ^{4,5} with a broad range of applications. ^{6–9} So far permanent and electromagnetic devices have been extensively employed although different solutions, e.g. based on channeling, ^{10,11} have been proposed. Superconducting magnets ¹² are at the edge of present technology and NbTi superconductors cooled at cryogenic temperatures represent the state of the art. They are routinely used, for instance, at the Large Hadron Collider (LHC) where more than 2/3 of the 27 km-long ring is filled by 8 T superconducting dipole magnets ^{13,14} for the bending of the 7 TeV proton beams. With current limits of superconducting technology, it is difficult to envision compact solutions that can be scaled to even greater energies and/or larger deflection angles.

In this context plasma technology represents an alternative approach. Plasmas can sustain extremely large fields¹⁵ and currents^{16–19} and, for these reasons, they are replacing conventional accelerators^{20–22} and standard focusing devices.^{23–25} Recently, several proof of principle experiments have been performed in focusing electron beams by means of the so-called active plasma lenses, ^{26–28} schematically depicted in Fig. 1. They consist of gas-filled capillaries in which the plasma is produced by an electrical discharge.^{29,30} According to the Ampere law, an azimuthal magnetic field B_{ϕ} is induced across the capillary whose strength increases radially and, unlike standard quadrupoles, provides symmetric focusing of the beam in both transverse planes. Here we show that the same mechanism can also be used to deflect particles. In the active plasma lens the Lorentz force produced by the azimuthal magnetic field pushes the travelling particles toward the capillary axis (where it vanishes) and the same applies for curved shapes since the flux of plasma electrons driven by the discharge actually follows the capillary geometry.^{31,32} Such a device, hereinafter called Active Bending Plasma (ABP), presents interesting features when considering the effects of deflection on the particle



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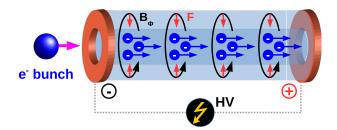


FIG. 1. Scheme for particle guiding. A discharge current flows through the plasma capillary inducing, according to the Ampere law, an azimuthal magnetic field \mathbf{B}_{ϕ} whose resulting force \mathbf{F} focuses an externally injected electron bunch.

beam and can in principle reach greater magnetic fields (and, thus, larger deflection angles) than superconducting magnets. In the paper we present the main features of such a device and a detailed study based on numerical simulations both for the particle guiding and plasma dynamics.

To test the guiding efficiency of the ABP we will refer to a reference electron beam with 50 pC charge, energy E = 100 MeV (0.1% energy spread), 1 ps duration (or, equivalently, $\sigma_z \approx 300 \ \mu m$ length), $\epsilon_n = 1 \ \mu m$ normalized emittance and $\sigma_{x,y} = 100 \ \mu m$ spot size. All the quantities are quoted as root mean square (rms). The particle trajectories are reconstructed by using the General Particle Tracer (GPT) code³³ while the bunch dynamics along the plasma channel is investigated with Architect, a hybrid-kinetic fluid code. 34,35 Similarly to the active plasma lens, ABP requires a magnetic focusing field whose strength increases with radius. When the bunch particles move away from the axis they experience a larger recalling force pushing toward the center of the capillary. The required magnetic field can be obtained with the so-called capillary discharge waveguides, ^{29,30} in which a discharge current is pulsed through a capillary pre-filled with gas.

Under these assumptions, we have tested the feasibility of the ABP concept by employing a bent capillary with $R_c = 1$ mm hole radius and $\rho = 10$ cm radius of curvature. For the chosen parameters the bending requires at least a magnetic field with strength $B_{\phi} = \beta E c/q_e \rho \approx 3.3$ T, where β is the bunch velocity normalized to the speed of light c and q_e is the electron charge. The magnetic field radial profile $B_{\phi}(r)$ across the capillary is calculated with a one-dimensional analytical model that assumes the plasma distribution as a balance between Ohmic heating and cooling due to electron heat conduction. 36 The model computes the plasma temperature profile T(r) allowing to retrieve its electric conductivity $\sigma_e(r)$ and, in turn, the current density J(r) flowing through it. The resulting magnetic field is then calculated according to the Ampere law as $B_{\phi}(r) = (\mu_0/r) \int_0^r J(r')r'dr'$, with μ_0 the vacuum permeability.

Fig. 2(a) shows the radial magnetic field for a discharge current of $I_D = 25$ kA to a capillary pre-filled by pure Hydrogen gas with 10¹⁹ cm⁻³ density. On the same plot we also report temperature and density profile as a function of the radial coordinate. The resulting vector plot of the magnetic field lines is shown in Fig. 2(b). The gas and density have been chosen to avoid plasma pinching and maintain a pure Ohmic regime. In these conditions the average plasma temperature and electron density are $T_e \approx 17 \text{ eV}$ and $n_e \approx 7 \times 10^{18} \text{ cm}^{-3}$. Being the plasma thermal pressure (per volume unit) $p_T = 4N_e k_B T_e$ (with k_B is the Boltzmann constant and $N_e = n_e \pi R_c^2$ the number of electrons per unit length) and the magnetic pressure $p_B = \mu_0 I_D^2 / 4\pi$, it is $p_T \gg p_B$ and thus no pinching is expected.³⁷ For the sake of completeness we have numerically cross-checked such a statement by employing the so-called "snow-plow" model³⁸ that analyses the plasma dynamics under the influence of the external discharge circuit. The results confirm that no pinching occurs by using the same plasma parameters

The magnetic field of the ABP in the full three-dimensional space is then computed with the commercial code CST STUDIO,³⁹ that computes the field map along the curved capillary geometry by using the previously obtained electrical conductivity $\sigma_e(r)$. Fig. 2(c) shows the resulting intensity profile along the y = 0 plane. Two 1 cm long straight sections have been included before and after the curved capillary.

To test the particle deflection, we imported the 3D field map into GPT. The reference electron beam, consisting of 10⁶ macro-particles, is assumed to be injected from the left of Fig. 2(c)

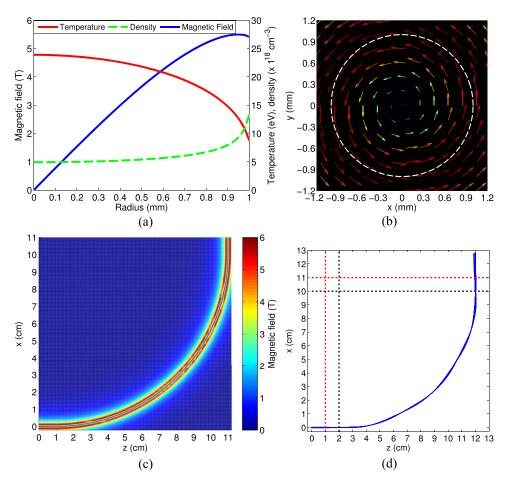


FIG. 2. (a) Calculated radial profiles of the magnetic field (blue), temperature (red) and electron density (green) in a pre-filled Hydrogen capillary for $I_D = 25$ kA discharge current. (b) Vector plot showing the field lines in the transverse x-y plane. The white dashed circle indicates the capillary walls. (c) Magnetic field intensity (along the y = 0 plane) for the bent capillary with $\rho = 10$ cm curvature radius. Two 1 cm-long straight sections are included before and after the bent path. (d) Trajectories of the travelling electrons along the curved path. The red (black) dotted lines show the capillary channel (without) including the two straight sections. A drift of 1 (2) cm is considered in the simulation upstream (downstream) the capillary channel.

at x = y = z = 0. The simulated macro-particle trajectories are reported in Fig. 2(d). An initial (final) drift of 1 (2) cm is considered upstream (downstream) the capillary channel. The red (black) dotted lines show the overall path (without) including the two straight sections. The plot highlights that all the particles are properly bent and follow the curved path along the capillary. The beam envelopes are shown in Fig. 3. Here we refer to the envelopes $\sigma_{x',y',z'}$, i.e. the ones calculated in the beam co-moving system x', y', z', with z' indicating the relative position along the curved path. The beam undergoes several betatron oscillations during its motion. These are evident by looking at the evolution of σ_y since such a plane is not affected by the deflection. Regarding the σ_x envelope, it exactly resembles σ_y up to the end of the straight capillary section (approximately at z' = 3 cm), then it follows a different behavior on the plane of deflection.

An interesting feature we can retrieve from Fig. 3 is the evolution of the bunch length σ_z . We can see that such a quantity is effectively preserved (within 1% of its initial value) at the end of the bending, thus no elongation (or longitudinal dispersion) of the bunch is observed as in the case of conventional bending magnets. It is due to the fact that, regardless of their energy, all the particles follow approximately the same path. By considering that the azimuthal magnetic field grows radially, larger (lower) is the particle energy larger (smaller) is the offset with respect to the reference path since $\rho \propto E$. As a consequence, a stronger (weaker) kick is produced, resulting in trajectories that are almost independent on the particle energies.

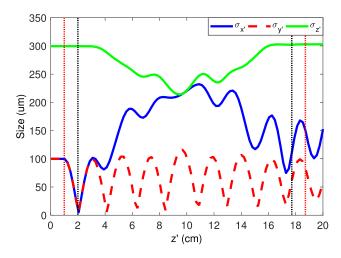


FIG. 3. Bunch envelopes as a function of the longitudinal position z'. The transverse sizes are labelled as $\sigma_{x',y'}$ (solid blue and dashed red lines). The bunch length is denoted by $\sigma_{z'}$ (green line). As in Fig. 2(d), the red (black) dotted lines show the capillary channel (without) including the two straight sections.

Fig. 4 compares the initial (+) and final (\circ) beam longitudinal phase space (LPS) as computed by the Architect code. At the end of the ABP a small fraction (less than 0.1%) of particles in the tail is weakly accelerated by the induced plasma wakefield but the main core of the bunch actually remains unaffected and the overall elongation is of the order of 0.4%. In the same plot we have also reported the resulting LPS at the exit of a conventional bending dipole (\times), modeled as a sector magnet with same radius of curvature ρ and gap equal to $2R_c$. In this case the bunch acquires an energy chirp and its elongation is more pronounced (about 8%).

A parametric study conducted on several beam configurations is summarized in Fig. 5. The effectiveness in preserving the length of even ultra-short bunches (down to 3 μm or, equivalently, 10 fs) is shown in Fig. 5(a) as a function of the bunch spot size at the ABP entrance. We can see that such a quantity is better preserved for small aspect ratio beams, i.e. when σ_x , $y/\sigma_z \lesssim 1$. In a similar study, reported in Fig. 5(b), we confirm that even with large energy spreads (up to 6%) the elongation is contained within only 5%. The same plot also highlights that, for a conventional bending dipole, the same energy spreads would result in an overall elongation approximately 200 times larger. The ability to guide the beam for different discharge currents flowing through the capillary is shown in

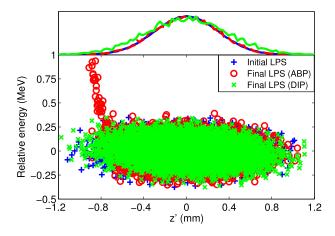


FIG. 4. Longitudinal phase space (LPS) at the entrance (+) and exit (\circ) of the ABP. The y-axis shows the single particle energies with respect to the mean bunch energy (100 MeV). The resulting LPS at the exit of a conventional bending dipole (\times) is also reported. On top the resulting histogram of the bunch longitudinal profile for the three cases is shown.

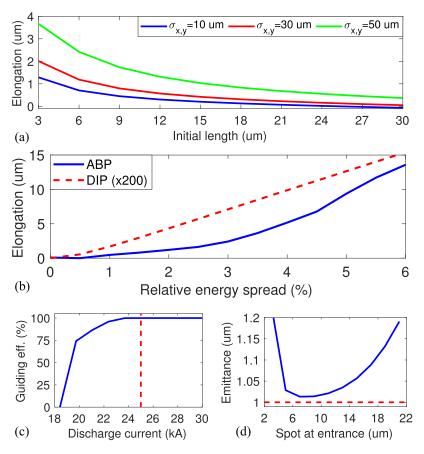


FIG. 5. (a) Bunch elongation as a function of the initial bunch length for several spot sizes at ABP entrance. (b) Elongation calculated at different energy spreads for the reference beam ($\sigma_z = 300 \, \mu m$) at the end of the ABP (blue line). The red dashed line refers to a conventional bending dipole. Its real values must be multiplied by a factor of 200. (c) Guiding efficiency as a function of the applied discharge current. At lower values a larger fraction of particles is lost. The red dashed line represents the discharge current used for all the calculations considered so far. (d) Resulting emittance at the end of the transport as a function of the initial spot size. The red dashed line indicates the initial emittance ($\epsilon_n = 1 \, \mu m$).

Fig. 5(c). For the reference 100 MeV beam, a minimum current $I_D \approx 24$ kA is needed to ensure the proper bending for all the particles. At lower currents the guiding is less efficient and a larger fraction of particles is lost during the transport. On the contrary, at larger currents the guiding is always guaranteed being the resulting magnetic field large enough to keep all particles on the reference trajectory. In Fig. 5(d) we have evaluated the emittance increase as a function of the spot size at capillary entrance. We observe that the beam emittance is preserved when $\sigma_{x, y} \ll R_c$, which ensures that the magnetic field (as the one calculated in Fig. 2(a)) is almost linear along the bunch radial profile. For the reference beam, instead, we find a dramatic emittance degradation (up to 40 μm) due to its large initial spot size.

In this context, the best scenario is obtained when the beam is matched with the focusing channel. By assuming a linear focusing force $F(r) = k^2 r$ (with $k^2 = \mu_0 q_e \beta c I_D / 2\pi R_c^2$) acting at distance r from the axis, the beam envelope equation is

$$\sigma_{x,y}^{\prime\prime} + k_n^2 \sigma_{x,y} = \frac{\epsilon_n^2}{\sigma_{x,y}^3} , \qquad (1)$$

where $k_n = k/\sqrt{\gamma m_e c^2}$ is the normalized lens focusing strength, γ the relativistic Lorentz factor and m_e the electron rest mass. The equilibrium solution is associated to a betatron oscillation of amplitude $\beta_{eq} = 1/k_n$ and thus to a matched spot size equal to $\sigma_{eq} = \sqrt{\beta_{eq} \epsilon_n/\gamma} \approx 7 \ \mu m$. For such a value we achieve the emittance minimum in Fig. 5(d).

In conclusion, we have presented a new device based on a capillary-discharge waveguide able to deflect particles at large angles. The theoretical treatment is discussed and supported by numerical simulations showing that the guiding, under certain conditions, preserves both the beam emittance and longitudinal phase space. The latter feature, in particular, would be particularly useful in accelerator facilities. If the beam has to be translated in a different beamline, a system consisting of (at least two) consecutive bending magnets separated by dispersion-matching focusing optics (e.g. quadrupoles and sextupoles) has to be adopted to preserve (or compress) the bunch duration. 40,41 On the contrary, by means of the ABP even ultra-short beams can be transported without requiring additional optics. We have also demonstrated its capability in guiding particle beams with large energy spread as, for instance, the ones coming from plasma-based accelerators. 42–44 In such a specific case the transport up to a specific location would represent a tricky task to accomplish when employing conventional magnetic optics (strongly affected by chromatic effects). With the ABP, instead, the overall elongation would be contained within only few percent.

Regarding its scalability to larger beam energies (and/or larger deflection angles), the ABP can still be used by tuning its main parameters (radius of curvature, discharge current and capillary radius). Here we have demonstrated how to obtain the most compact structure able to bend by 90° a 100 MeV electron beam. For all the other cases, e.g. when dealing with larger energies, the radius of curvature has to be increased (since $\rho \propto E$) by employing longer capillaries and avoiding the use of too large discharge currents that can induce plasma pinch and other nonlinear effects. If compared to the state of the art of current technology, based on superconducting magnets operating at cryogenic temperatures, its practical implementation would be simpler and affordable in terms of costs. The ABP might thus represent an alternative solution to develop more compact beamlines and, in general, to bend and guide charged particle beams.

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