Education and research in Computer Aided Architectural Design in Europe

# eCAADe 2013 Computation and Performance 18-20 September, 2013

**Delft University of Technology** 

Volume 2

**Edited by Rudi Stouffs and Sevil Sariyildiz** 

### Editors

Rudi Stouffs<sup>\*</sup> Sevil Sariyildiz Design Informatics, Department of Architectural Engineering + Technology, Faculty of Architecture, Delft University of Technology, Delft, The Netherlands (\* Department of Architecture, School of Design and Environment, National University of Singapore, Singapore)

1<sup>st</sup> Edition, September 2013

Computation and Performance – Proceedings of the 31<sup>st</sup> International Conference on Education and research in Computer Aided Architectural Design in Europe, Delft, The Netherlands, 18-20 September 2013, Volume 2. Edited by Rudi Stouffs and Sevil Sariyildiz. Brussels: Education and research in Computer Aided Architectural Design in Europe; Delft: Faculty of Architecture, Delft University of Technology.

ISBN 978-94-91207-05-1 (eCAADe)

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Publisher: eCAADe (Education and research in Computer Aided Architectural Design in Europe) and Faculty of Architecture, Delft University of Technology

www.ecaade.org

Cover design: Bige Tunçer and Rudi Stouffs Cover photograph: Ifigeneia Dilaveraki

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# eCAADe 2013

# **Computation and Performance**

Volume 2

Proceedings of the 31<sup>st</sup> International Conference on Education and research in Computer Aided Architectural Design in Europe

> 18-20 September 2013 Delft, The Netherlands Faculty of Architecture, Delft University of Technology

> > http://ecaade2013.bk.tudelft.nl/

Edited by Rudi Stouffs Sevil Sariyildiz

# Theme

# **Computation and Performance**

This is the second volume of the conference proceedings of the 31<sup>st</sup> eCAADe conference, held from 18-20 September 2013 at the Faculty of Architecture of Delft University of Technology in Delft, the Netherlands. Both volumes together contain 150 papers that were submitted and accepted to this conference.

The theme of the 31<sup>st</sup> eCAADe conference is the role of computation in the consideration of performance in planning and design.

Since long, a building no longer simply serves to shelter human activity from the natural environment. It must not just defy natural forces, carry its own weight, its occupants and their possessions, it should also functionally facilitate its occupants' activities, be aesthetically pleasing, be economical in building and maintenance costs, provide temperature, humidity, lighting and acoustical comfort, be sustainable with respect to material, energy and other resources, and so forth. Considering all these performance aspects in building design is far from straightforward and their integration into the design process further increases complexity, interdisciplinarity and the need for computational support.

One of the roles of computation in planning and design is the measurement and prediction of the performances of buildings and cities, where performance denotes the ability of buildings and cities to meet various technical and non-technical requirements (physical as well as psychological) placed upon them by owners, users and society at large.

This second volume contains 75 papers grouped under eleven subthemes that vary from *Simulation, Prediction and Evaluation over Models of Computation: Human Factors* to *Languages of Design*.

Rudi Stouffs and Sevil Sariyildiz

# Acknowledgements

With the 31st eCAADe conference held in Delft, eCAADe has finally come full circle. The very first eCAADe conference, before the actual founding of the eCAADe organization in 1983, was held in Delft in 1982. 31 years later, we are proud to welcome the eCAADe organization back to its origins.

This Delft conference has been a while in the making. The idea was first raised by Martijn Stellingwerff in 2006 and a preliminary proposal was presented to the eCAADe council at that time. However, we encountered some turbulent times with the destruction by a fire of the Faculty of Architecture building in Delft in 2008 and only in 2010 were we ready to present a definitive proposal for the conference in Delft. From that time until the publication of these proceedings, many people helped to make this happen and we hope to mention them all here:

First of all, we would like to thank both deans, Wytze Patijn (in 2010) and Karen Laglas (since 2011), for their endorsement and support, and especially the director of International Affairs at that time, Agnes Wijers, for her immediate support upon approaching her with the idea and for her ample support in the early planning of the conference event.

The eCAADe council was supportive throughout the entire process and helped with many aspects of the organisation. Both presidents, Wolfgang Dokonal (up to 2011) and José Duarte (since 2011), were very supportive. Bob Martens, as liaison with the conference host, was particularly helpful with many issues in the process. We received especially a lot of support from Henri Achten as previous conference organiser. Martin Winchester made sure the OpenConf system was running smoothly and reliably. Nele de Meyere and Maaike Waterschoot reacted promptly when approached with administrative questions. Financial support was generously provided by the sponsors Autodesk and Bentley Systems.

The Call for Extended Abstracts yielded 287 submissions. Fortunately, we were able to count on 135 international reviewers in helping us to assess all submissions (see the List of Reviewers section). Each submission was double-blind reviewed by three reviewers. Following the reviewers' recommendations, 150 papers were finally accepted for publication and presentation. We congratulate the authors for their accomplishment. Next to the authors, the reviewers, who volunteered valuable time and effort, the session chairs, who led the presentations, and the students and other volunteers, who assisted throughout the conference and its preparations, deserve our sincere thanks and acknowl-edgements.

As conference chairs, we had the support from the organising committee, including, Kas Oosterhuis, Joop Paul, Bige Tunçer, Martijn Stellingwerff, Michael Bittermann, Michela Turrin, Paul de Ruiter, Nimish Biloria and Henriette Bier. Joop Paul deserves a special note for securing Gerard Loozekoot, director of UN Studio, as keynote speaker. A special thanks goes to Irem Erbas, who, next to Bige Tunçer, Nimish Biloria and Michela Turrin, assisted in processing part of the proceedings. The secretarial team of the department of Architectural Engineering + Technology assisted on numerous occasions and Françoise van Puffelen, in particular, especially assisted in all financial matters. Thijs Welman secured the website and Martijn Stellingwerff designed the conference website. From the faculty we furthermore want to thank the FMVG (Facility Management and Real Estate) people who helped with the planning of and preparations for the event.

We are very grateful to have as keynote speakers at the conference Sean Hanna (as prominent

academic in the area of computation and performance), Shrikant Sharma (leader of SMART Solutions – Buro Happold's specialist service offering advanced computational solutions to practice) and Gerard Lozekoot (director and senior architect at leading Dutch architectural firm UN Studio) to provide their views on computation and performance to the conference.

We wish to provide a special acknowledgement to Yunn Chii Wong, head of the Department of Architecture at the School of Design and Environment, National University of Singapore, and Chris Magee, co-director of the SUTD-MIT International Design Centre, for offering their support to Rudi Stouffs to chair the preparations of this conference from abroad.

Finally, we want to thank Bige Tuncer, partner and colleague, and our families for their support and patience while we were spending late hours organising, reviewing, editing, and trouble shooting during the past three years.

eCAADe 2013 Conference Chairs Rudi Stouffs and Sevil Sariyildiz

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# Contents

- 5 Theme
- 7 Acknowledgements
- 9 List of Reviewers
- 11 Keynote Speakers
- 13 Contents

### 19 Simulation, Prediction and Evaluation

- 21 Using Smart Controlled AC and Ceiling Fan to Save Energy Pin-Hung Wang, Jui-Yen Lin
- 29 Even 'Clouds' Can Burn Antonio Fioravanti, Eolo Avincola, Gabriele Novembri
- **39** Inductive Aerodynamics Samuel Wilkinson, Sean Hanna, Lars Hesselgren, Volker Mueller
- 49 Adaptive Fluid Lens and Sunlight Redirection System Florian Heinzelmann, Telesilla Bristogianni, Patrick Teuffel
- 59 Modelling and Simulating Use Processes in Buildings Davide Simeone, Yehuda E. Kalay, Davide Schaumann, Seung Wan Hong
- 69 Flexing Wind Rafael Moya, Flora Salim, Mani Williams, Kamil Sharaidin
- 79 Real-time Environmental Feedback at the Early Design Stages Greig Paterson, Sung Min Hong, Dejan Mumovic, Judit Kimpian
- 87 DesignScript: Scalable Tools for Design Computation Robert Aish
- 97 Performative Design
- 99 Architectural Thermal Forms Isak Worre Foged
- **107 DaylightGen: From Daylight Intentions to Architectural Solutions** Mohamed-Anis Gallas, Gilles Halin
- **117 Performance Driven Design and Design Information Exchange** Sina Mostafavi, Mauricio Morales Beltran, Nimish Biloria
- 127 Performance Based Pavilion Design Sevil Yazici

- **137 Engineering Performance Simulations in Architectural Design Conception** Michela Turrin, Ioannis Chatzikonstantinou, Martin Tenpierik, Sevil Sariyildiz
- 147 Passive Energy Devices in Ceramics Mark Weston, Dan Greenberg

# 153 Generation, Exploration and Optimisation

- **155 Automated Simulation and Study of Spatial-Structural Design Processes** Juan Manuel Davila Delgado, Herm Hofmeyer
- **165** Generative Agent-Based Design Computation Ehsan Baharlou, Achim Menges
- **175 Evolutionary Energy Performance Feedback for Design (EEPFD)** Shih-Hsin Eve Lin, David Gerber
- 185 Cloud-Based Design Analysis and Optimization Framework Volker Mueller, Tiemen Strobbe
- **195** Graphical Smalltalk with My Optimization System for Urban Planning Tasks Reinhard Koenig, Lukas Treyer, Gerhard Schmitt
- 205 Evo-Devo in the Sky Patrick Janssen

## 215 Algorithmic Design Generation

- **217** The Potential of Evolutionary Methods in Architectural Design Wassim Jabi, Barbara Grochal, Adam Richardson
- 227 Genetic Algorithms Applied to Urban Growth Optimization Patricia Camporeale
- **237 Design Tools for Integrative Planning** Stefana Parascho, Marco Baur, Jan Knippers, Achim Menges
- 247 Infections Tuğrul Yazar, Fulya Akipek
- 255 Algorithmic Engineering in Public Space Jaroslav Hulin, Jiri Pavlicek
- 261 Integrating Computational and Building Performance Simulation Techniques for Optimized Facade Designs Mahmoud Gadelhak

- 271 Models of Computation: Form Studies
- 273 Algorithmic Form Generation for Crochet Technique J. Gozde Kucukoglu, Birgul Colakoglu
- **3D Regular Expressions Searching Shapes IN Meshes** Gabriel Wurzer, Bob Martens, Katja Bühler
- 289 A Computational Method for Integrating Parametric Origami Design and Acoustic Engineering Tsukasa Takenaka, Ava Okabe
- 297 A Novel Method for Revolved Surface Infrastructures Gökhan Kınayoğlu
- **305 Ruling Im/Material Uncertainties** Zeynep Akküçük, Mine Özkar
- **315 Hyperdomes** Andrea Rolando, Domenico D'Uva
- 325 Action Based Approach to Archaeological Reconstruction Projects: Case of the Karnak Temple in Egypt Anis Semlali, Temy Tidafi, Claude Parisel

- 333 Models of Computation: Human Factors
- **335** Fusion of Perceptions in Architectural Design Ozer Ciftcioglu, Michael S. Bittermann
- **345 Ambient Surveillance by Probabilistic-Possibilistic Perception** Michael S. Bittermann, Ozer Ciftcioglu
- **355 The Jacobs' Urban Lineage Revisited** Claudio Araneda
- 365 Collaborative and Human Based Performance Analysis Mathew Schwartz
- **375 Visibility Analysis for 3D Urban Environments** Anastasia Koltsova, Bige Tuncer, Gerhard Schmitt
- **385 Human Activity Modelling Performed by Means of Use Process Ontologies** Armando Trento, Antonio Fioravanti

## 395 3D Model Performance

- **397** New Methods for the Rapid Prototyping of Architectural Models Stefan Junk, Samantha Côté
- 405 Four Chairs and All the Others Eigenchair Miro Roman
- 415 Digital Design Tools versus Architectural Representation and Design Approach Betül Orbey, Nihan Gürel
- 425 Considering Physicality in Digital Models Andrzej Zarzycki
- 435 Understanding and Managing the Constructive Characteristics of Vernacular Architecture

Danilo Di Mascio

- 445 3D Digitization in Architecture Curriculum Luís Mateus, Victor Ferreira
- **453 Performing the Past and the Present for the Knowledge of the Future** Anetta Kepczynska-Walczak

# 463 Building Information Modelling

- **465 Challenges of Integrating BIM in Architectural Education** Tuba Kocaturk, Arto Kiviniemi
- **475** Attaining Performance with Building Information Modelling Eleni Papadonikolaki, Alexander Koutamanis, J. W. F. (Hans) Wamelink

#### 485 Building Your Own Urban Tool Kit Caner Dolas, Andreas Dieckmann, Peter Russell

- **495** [Architectural] Reasoning over BIM/CAD Database Gianluigi Loffreda, Antonio Fioravanti, Luigi Avantaggiato
- **505 Experiencing BIM Collaboration in Education** Stefan Boeykens, Pauline De Somer, Ralf Klein, Rik Saey
- 515 Landscape Information Modeling Veronika Zajíčková, Henri Achten
- 525 ifcModelCheck Sebastian Ebertshäuser, Petra von Both
- 535 Daylight Performance Simulations and 3D Modeling in BIM and non-BIM Tools Marina Stavrakantonaki

# 543 CAAD Curriculum

- 545 How to Teach 'New Tools' in Landscape Architecture in the Digital Overload Pia Fricker, Christophe Girot, Georg Munkel
- 555 150 000 Parametric Control of PET Bottle Structure Kateřina Nováková, Lukáš Kurilla, Henri Achten
- 563 Identifying Cognitive Operations of Conception Implied in the Uses of Parametric Modeling in Architectural Design: Toward Pedagogical Tools Aurélie de Boissieu, François Guéna, Caroline Lecourtois
- 571 Continuous Oscillations Günter Barczik
- 579 Computation/Performance Anna Pla-Catala
- 587 Dances with Architects Angelika Lückert, Volker Koch, Petra von Both
- 595 A Case Study in Teaching Construction of Building Design Spaces Mahsa Nicknam, Marcelo Bernal, John Haymaker
- 605 Innovative Learning for Collaborative Design in Ergonomics Viviane Folcher, Khaldoun Zreik, Samia Ben Rajeb, Pierre Leclercq

# 615 Shape Grammars

#### 617 Unambiguity Thomas Grasl, Athanassios Economou

- 621 Customized Cork Façade Rui Marques, Sara Eloy
- 627 A Generative Approach towards Performance-Based Design Tiemen Strobbe, Ronald De Meyer, Jan Van Campenhout
- 635 Tableware Shape Grammar Eduardo Castro e Costa, José Pinto Duarte
- 645 Grandstand Grammar and its Computer Implementation Yimin Sun, Lu Xiong, Ping Su
- **655** From Point Cloud to Shape Grammar to Grammatical Transformations Filipe Coutinho, Luis Mateus, José P. Duarte, Victor Ferreira, Mário Kruger

### 665 Languages of Design

- 667 Combining Complexity and Harmony by the Box-Counting Method Wolfgang E. Lorenz
- 677 The Rehabilitation Design Process of the Bourgeois House of Oporto: Shape Grammar Simplification Eugénio Coimbra, Luís Romão
- **687** Albertian Grammatical Transformations Bruno Figueiredo, José Pinto Duarte, Mário Krüger
- 697 A Parametric Recreation of Traditional Chinese Architecture Di Li, Michael Knight, Andre Brown
- 705 A Bottom-Up Social Housing System Described with Shape Grammars Leticia Teixeira Mendes, José Nuno Beirão, José Pinto Duarte, Gabriela Celani
- 715 The Language of Mozambican Slums Pedro Barros, José Beirão, José Pinto Duarte
- 725 Gulou Structure Grammar and its Computer Implementation Lu Xiong, Wei Xiong, Hongxia Zhang
- 735 Index of Authors

# **Even 'Clouds' Can Burn**

# Fire engineering simulation for a safe, innovative and high-performance architectural design - a case study

<u>Antonio Fioravanti</u><sup>1</sup>, Eolo Avincola<sup>2</sup>, Gabriele Novembri<sup>3</sup> Dept. DICEA - Sapienza University of Rome, Italy <sup>1.3</sup>http://www.dicea.uniroma1.it <sup>1</sup>antonio.fioravanti@uniroma1.it, <sup>2</sup>eoloavincola@gmail.com, <sup>3</sup>gabriele.novembri@ uniroma1.it

**Abstract.** Architecture, nowadays, is an even more demanding activity in which complexity is the keyword: complex forms, complex functions and complex structures require sophisticated facilities and components, for example, 'The Cloud' of D. and M. Fuksas in Rome. These complexities can give rise to numerous risks, among which fire is frequently a central problem.

The fire safety norms do not involve an approach integrated with other instruments or building model (BIM), but provide a list of information and constraints. These codes are now shifting away from a prescriptive-based towards a performance-based method due to recent progress in fire safety engineering.

Following this approach, a case study simulation of a multi-purpose centre was carried out in Tivoli, near Rome. This simulation allowed greater freedom in architectural composition, a lower risk to people, a larger number of material and building components used and higher safety standards to be achieved. The model is based on the FDS (Fire Dynamics Simulator) language, a simulation code for low-speed flows, focused on smoke, particle and heat transport by fire.

**Keywords.** *Architectural design; computational fluid-dynamics; fire propagation; fire safety; smoke propagation.* 

#### FIRE AND ARCHITECTURAL DESIGN

Architecture has always been a demanding activity, but in present times, has had to face intertwined problems in which complexity is the keyword: complex forms, complex functions and complex structures require sophisticated facilities and components. These complexities can give rise to numerous risks, among which fire is frequently a central problem (Harper, 2004). Existing fire safety regulations and codes (Balaban et al., 2012) very often actually represent as many limitations imposed on architectural needs such as space layout, free form space, distribution path, space occupancy and aesthetic quality. Fire safety, more specifically smoke and heat extraction, requires optimization and careful analysis in the early design phases. These norms are the average of real fire safety cases, and so in some specific cases, they are more demanding than strictly necessary with regard to devices or shape layout, while in others they could actually be insufficient.

An impressive example of the impact of fire regulations on architecture is represented by the recent design competition for the new Rome Conference Centre in 1998. It is situated near the old one, in the district of the Esposizione Universale Roma - EUR (Rome Universal Exhibition) planned for 1942 where, according to Mussolini's town plan, important ministries would subsequently be transferred. The old Conference Centre was designed by Adalberto Libera in 1939 and is a reflection of late Italian rationalist style tinted with a superficial, ironical and monumental classicism. There were numerous important responses to the 1998 competition call and several high quality projects were selected. Many were based on mimicking the symmetrical and constrained layout resulting from a simplistic interpretation of the apparently elementary nature of the EUR buildings. Another important motivation was the difficulty to take into account current safety rules regarding structure, plant engineering and evacuation paths in a free form space configuration.

In many cases, this design logic led to the various conference halls being situated as low as possible and for fire fighting purposes to use water cisterns (filled with water) at the top of the building. These design solutions had the following consequences: overloading at the building top, which is a design solution to be avoided in view of the seismic nature of Italian territory; an obstruction of the visual permeability between inside and outside in order to respect the fire resistance of the walls; the denial of whole roof level availability and limited panoramic view due to the presence of cisterns. Other examples are: the Twin Towers, which had cisterns on the roof that unfortunately failed to cope with the combined effect of fire and the abrasion of the intumescent paint protecting the steel structure; or the first HKSBC projects in which water inside the pillars was thought to cool the structure at the price of adding permanent loads.

The engineering approach makes it possible to exceed the limits prescribed by the codes and at the same time rigorously respect safety as the norms regulate only average scenarios. This approach allows designers to have a greater compositional freedom, obtaining innovative and high-performance buildings in which fire safety has become an essential element of architectural conformation. In other words, fire engineering is used to allow fire safety to be demonstrated, despite its peculiar form and dimension like the new Congress Palace in Rome designed by D. and M. Fuksas - familiarly called "The Cloud" [1, 2]. In this case, it was possible to use fire engineering simulation techniques to demonstrate that the danger, in the case of fire, was very low as the space enclosed by the 'glass box' could be considered an open space and as the thinness of the membrane enveloping 'The Cloud' renders the fire load negligible.

This approach has allowed modifications to be avoided during the detailed building design phase that might compromise the identity of the project.

#### FIRE SAFETY PRESCRIPTIVE APPROACH

The combustion process is a sequence of chemical reactions between a fuel and an oxidant, accompanied by the production of heat, smoke and the conversion of chemical materials. The process can be specified by means of the Fire Triangle, which is composed of fuel, oxygen and a heat source. It is essential for a correct relationship among these three elements otherwise, combustion itself cannot take place (Harper, 2004).

Inside a *compartment* - i.e. a homogeneous and limited part of the building with respect to function, use destination and fire safety class - it is possible to identify four fire phases (La Malfa, 2009):

*Ignition*, a heat source acts on the fuel, and if sufficient thermal capacity is released, it warms it up to its ignition point. The thermal energy needed to attain the ignition temperature depends on size and the ratio between the mass and the surface exposed to the air.

Growth, the fuel materials are heated and tend

.





to reach their ignition temperature. The spread of the fire produces: a reduction in visibility, increased toxic fumes, increment of the burning rate over time.

- Development, all combustible materials in the compartment are simultaneously involved in the burning process due to the irradiation caused by the products of combustion: the "flashover" phenomenon.
- Decay, the fire tends to slow down owing to the progressive reduction of combustible materials or oxygen and starts to be extinguished.

Codes do not involve an integrated approach nor do advanced CAD tools like building information modelling - BIM, but they do provide a list of documentations and prescriptions to be fulfilled, which are useful in the early design phases (Balaban et al., 2012):

- Definition of project, detailed description of building with particular reference to ventilation openings, fire and smoke compartments, structure and distribution of furniture and combustible materials;
- Fire safety objectives and indication of performance requirements, in relation to specific architectural goals and to requirements for which the analysis is applied (maximum gas temperature at human head height, visibility, air concentration of toxic substances);
- Determination of fire scenarios, schematizing events that may occur in relation to the characteristics of fire, the building and the occupants;

Method of contrast, for the achievement of the safety objectives set (obstacles to combustion product propagation, smoke devices, fire extinguishing systems and fume extractors);

#### FIRE SAFETY PERFORMANCE APPROACH

Building codes are shifting from a *prescriptive-based* method towards a *performance-based* method due to the progress in fire safety technologies, including the development of an engineering approach (McGrattan et al., 2010; Hadjisophocleous and Benichou, 1999). The traditional *prescriptive* method uses a set of technical standards that are rigidly applied in a 'mechanical' way. The *performance* method allows the actual risks for specific activities to be evaluated step-by-step by means of careful analysis and simulation.

In Italy, the engineering approach to fire safety is regulated by laws, the most important of which (D.M., 2007) defines the procedural aspects and criteria for assessing the level of risk and consequently the mandatory design measures intended to contrast possible code violations.

#### Heat Release Rate Parameter

The *Heat Release Rate* - HRR - is the main parameter governing the fire phenomenon; it influences many other fire characteristics. Literally, the HRR indicates the heat released by the combustion of a material over time per unit surface area (Babrauskas, 1991).

The area under the curve (Figure 1) represents the energy released during all *phases*, while, for the purpose of fire safety, it is essential to evaluate the phase preceding the *flashovers*, because after this time conditions are created that are unsustainable for the human body.

For this reason, it is necessary to know the variation over time of the actual *fuel mass involved* which, in the *growth phase* of the fire, is expressed by the equation (1). It displays different curves pertaining to fire growth (Figure 2) depending on the time "t" by means of a quadratic function and on the constant " $\alpha$ " that takes into account different material types. The combustion speed can be: *slow*,  $\alpha = 2.77$   $\times 10^{-3}$  KJ/s<sup>3</sup>; medium,  $\alpha = 11.11 \times 10^{-3}$  KJ/s<sup>3</sup>; fast,  $\alpha =$  $44.44 \times 10^{-3}$  KJ/s<sup>3</sup>; ultra-fast,  $\alpha = 177.77 \times 10^{-3}$  KJ/s<sup>3</sup> (La Malfa, 2009). (1)

 $HRR = \alpha \times t^2$ 

The curves do not grow indefinitely, but reach a peak and then begin to decrease, so the quadratic part refers only to the crescent monotonic curve. The decay phase, for common materials, accounts for 20÷30 % of the whole combustion process.

Curve peak values change according to the material being burnt. For example, plastic rubbish has a peak of 80 KW, while a car can reach 6000 KW.

As the HRR increases, also the temperature and the rate of temperature rise increase, thus accelerating fire development. In addition, increased HRR results in reduced oxygen concentration and increased production of gaseous and particulate matter; these are fundamental factors to be considered for fire safety.

#### Material Reaction Rate to Fire

For a given material, the reaction can produce a solid, denoted as residue, plus water vapour and/or fuel gas; for instance, the evaporation of water from a solid material is described by the reaction that converts liquid water-to-water vapour (McGrattan et al., 2010).

A pyrolyzing solid in a reaction produces a solid residue, water vapour and fuel gas, the sum of which has the same weight; this means that the mass of the reactant is conserved.

Another important parameter to consider is the mass fraction that can be burnt at time "t" (Figure 3, blue curve) of the normalized density of material, which decreases as the sample is slowly heated. The reaction rate (Figure 3, green curve) is the rate of change of the mass fraction at time "t"; where this curve peak is referred to as the reference Temperature "T," which is not the same as the ignition temperature, but is the most important parameter for defining the *reaction rate* of a material.

Equation (2) defines the reaction rate - "r" - at reference Temperature T<sub>e</sub> [°C], of the -i<sup>th</sup> material undergoing its -j<sup>th</sup> reaction; Y<sub>e</sub> defines the ratio between





the density of the -ith material component of the layer at temperature T, divided by the initial density of the laver.

$$\mathbf{r}_{ij} = \mathbf{A}_{ij} \times \mathbf{Y}_{s,i} \times \exp\left(-\frac{\mathbf{E}_{ij}}{\mathbf{BT}_{s}}\right) \tag{2}$$

The model used is based on the FDS (Fire Dynamics Simulator) language, a simulation code for low-speed flows, focused on smoke, particle and heat transport by fire. This model provides the estimation of the fire's evolution, dividing the space into a large number of small contiguous elements where the thermodynamic state is calculated by solving the conservation equations of mass, energy, etc. (Ozel, 1998). methods and analysis of results, the field

This approach allows the problem to be solved by integrating a set of partial differential equations for the whole system, thus avoiding the explicit treatment of the boundary conditions. One of the





#### Figure 4

Case study of a multi-purpose exhibition centre at Tivoli - the conference hall. The dashed blue lines define the compartment and the BEAM devices measure the total obscuration rate between two points.



main calculation problems is the actual choice of mesh: decreasing the size of the elements, a more realistic simulation is obtained, although this requires a longer computation time and greater hardware power.

The mathematical model used for solving the analysis of fire phenomenon and interface problems among contiguous space elements is the *phase field* model (Boettinger et al., 2002) that, by means of a specific and infinitesimal mesh, can correct dynamic interface problems.

#### MULTI-PURPOSE EXHIBITION CENTRE AT TIVOLI - CASE STUDY

The case study was an experimental master's degree thesis of a project for a multi-purpose exhibition centre with a multi-storey underground parking station in Tivoli, near Rome; the simulation was focused on the *compartment* of the conference hall (Figure 4).

The fundamental value to be specified was, as previously mentioned, the *Heat Release Rate* - HRR. This was schematized with a *burner*, on which a *vent* 

was applied, which simulated a fire that released heat but also a specific quantity of *particles* and *gas*, based on input data. The levels of HRR developed from the case study are based on information derived from the experimental data and compared with the values identified in the technical literature for those specific activities.

In the case of a multi-purpose hall, the presence of scene panels is assumed (Table 1) which increases the total fire load.

A rapid decrease of the HRR was observed due to the action of the simulated sprinkler system (automatic opening), giving a value of the fire extinction coefficient. This was made possible only through the correct sizing of the sprinkler piping, by indicating the flow of the single sprinkler obtained from the product specifications and the UNI regulations (UNI EN 12845, 2005).

Some fire scenarios of NFPA 101 (Coté and Harrington, 2012) were determined in compliance with the law (D.M., 2007). Relevant critical scenarios representative of the actual conditions were produced

Furniture type	[MJ/One]	Quantity	Sur.Compartment [m <sup>2</sup> ]
filing cabinet (included content)	2009	1	359
big lamps	160	30	359
small lamps	50	50	359
armchairs	335	206	359
secondary electrical panel	300	1	359
metal desk	837	1	359
chairs	67	2	359
big table	590	1	359
Product type	[MJ/m³]	Quantity [m³]	Sur.Compartment [m²]
electrical equipment	670	1	359
telephone and PC	200	1	359
electric cables	600	1	359
ceiling	1200	9	359
metal rods	800	2	359
sound-absorbing panels	6000	9	359
wood flooring	1200	9,2	359
wood doors	1800	0,6	359
spotlights/optical instruments	200	1	359
coating wall	1500	9	359
scenographic panels	3500	30	359
projection screen	1000	4	359

 Table 1

 Fire Load calculation in relation to the furniture or product type.

using: a preliminary check of regulations; expected performance levels; considering, for additional safety, the failure of the sprinkler system or devices for automatic door opening. It was also possible to simulate fire scenarios that are worse than the NFPA 101 code fire scenarios. Those could be the most severe fires ever recorded, or the average of the worst fires having occurred with some regularity. The fire scenarios were examined for a period of 10 minutes, an appropriate time for a preliminary investigation (Figure 5 and 6).

The choice of particulate *reaction rate* is one of the most critical aspects (Kittle, 1993): for example, in the pre-flashover phase, a modest amount of electrical equipment could spread smoke more dangerously than a common fire with greater reaction rate levels.

All the simulations verified the fire scenarios considered by analysing variations of: gas temperature at human head height and at construction element height (by temperature detectors - THCP); curve of heat release HRRPUA [KW/m<sup>2</sup>] derived from the sum of the value of the initial burner plus any contribution of fuel elements; visibility in the room for the egress time (by rate dimming detectors -BEAM); fume, particle and heat flow trends in the *compartment*; sprinkler operation.

The main architectural problems were encountered both:

- outside the building, the relationship with the square (quality of urban space)
- inside the building, the layout of the conference hall within the overall shape of the building (guality of architectural composition).

As far as the first point is concerned, namely the urban environment, two aspects must be taken into consideration which heavily affect the architectural composition and the cost of the building: the time required for firemen to arrive from the nearest fire station and the building conformation, which is linked to the constraints imposed by the underground parking safety openings. In the case of the Figure 5

Particle diffusion showed in a longitudinal section of the multi-purpose conference hall study case 5 minutes after fire ignition.





first aspect, the most important features are the non-combustible nature of the materials used and/ or the time needed for the bearing structure to resist until the fire fighters arrive. This aspect seems to be mainly dependent on the materials used and to exclude any reference to the 'form'. In actual fact the shape of the building, of its interior and the accesses to it constrain the possible manoeuvres of



the fire fighting and rescue vehicles and the extinguishing of the fire. The second aspect, the shape of the building and of the surrounding area is directly affected by the large air wells required to make the underground parking levels comfortable and safe. It was observed that by simply applying the codes literally, these 'wells' heavily affected the restaurant area, unless the latter was shifted further north and thus could not be used in the winter. However, applying the model to an alternative proposal for the location of the 'wells' in such a way as to leave the positioning of the restaurant unchanged and simulating the fire process, it was possible to verify the safety.

As far as the second point is concerned, as for example the compartment of the multi-purpose hall, according to the code (UNI 9494-1, 2012), the smoke and heat exhaust openings must have a continuous surface as long as the corridor length at a height of over 1.2 meters, thus conditioning the compositional, formal and acoustical aspects. In addition, the facade would have to be constituted by solid and non-combusting materials with high temperature proofing. The simulation verified safety standards also with a less invasive action on architectural composition, thus allowing different materials and shape. The simulation computed that the required fresh air brought into the conference hall only through emergency doors was enough for people, for structural safety and for visibility even if the opening (doors and windows) size of the walls did not satisfy those codes. After an accurate simulation, glass façades were allowed as they would be shattered by the high temperature at the beginning of the fire process. This is dependent on the capacity of fire engineering simulation accurately to predict the fire status.

#### **CONCLUSIONS AND FUTURE PROSPECTS**

The simulation performed led to better use of the urban square (the prescriptive method imposed huge underground parking ventilation openings); more freedom in architectural composition (codes constrained doors and windows position and size); reduced risk to people; freedom in the use and choice of a larger number of materials, furniture and building components.

Moreover, if the traffic regulations governing the area outside the building were to change and cause a delay in the arrival of the fire fighting vehicles it would be possible to simulate the behaviour of the fire in the building to check whether in any case the safety of visitors and staff were guaranteed or whether any further action was necessary and the extent thereof. This simulation, extended to all the buildings affected by the change in traffic regulation, would entail at the town planning level a detailed estimate of the costs/benefits-safety ratio.

The main difficulty encountered in the use of the simulation model was due to the limited interface with other CAD programs as it exports only 3D (AutoCAD<sup>®</sup>, Blender<sup>®</sup>). The integration of this analytical model with BIM would be desirable, as has already been done with structural and thermal calculation programs. An integrated design could thus be totally exploited in the building process, thus facilitating collaboration and information exchange.

This study, which was developed in the form of an experimental master's degree thesis, should be included in an academic course. In Italy, although there are many post-graduate professional courses concerning the applications of fire safety, most academic students ignore fire safety problems, so they should be taught at least the main principles for fire safety and, secondly, those for high-performance buildings.

Nowadays, the buildings are often readapted through a change of use, resulting in fire load variation; besides the building codes are constantly changing, giving rise to maintenance and accommodation activities with additional costs not specified in the design process. Moreover, the relationship between the study of fire phenomena and architectural conformation becomes fundamental in historical buildings, where architectural restrictions and heritage preservation do not actually go hand in hand with fire safety needs. All these problems can be faced by means of the fire engineering simulation approach that allows performance evaluation during a building's lifetime.

Fire safety engineering should not be interpreted, in the narrow sense, as a tool allowing the prescribed regulations to be sidestepped, but as a system model that can analyse real cases in depth, afford more solutions to problems, achieve higher safety standards and a more accurate evaluation and analysis of the risk of fire, so as to reduce problems from the outset. For example, in Italy this approach, when adopted, has led to a new image of steel structures completely free of protective coatings (intumescent paintings or cement or stucco or aluminum and insulation panels), with evident savings in construction costs.

The performance-based method allows a preliminary evaluation during the design process, avoiding not only increased costs but also modifications that often distort the identity of the building.

The use of these tools during the various phases of new construction design or in rehabilitation projects regarding existing buildings or during a building's lifetime can allow designers and the competent authorities to collaboratively develop projects, ensuring enhanced security also at urban level. There are two possible future developments of these tools: a numerical one, through integration with other multi-physical tools (e.g. COMSOL®), or a semantic one using ontology tools and AI methodologies.

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# **Index of Authors**

#### Α Buš, Peter Achten, Henri 1-51, 1-213, 1-477, С 2-515, 2-555 Çağdaş, Gülen Aish, Robert 2-87 Camporeale, Patricia Akipek, Fulya 2-247 Canavezzi de Abreu, Sandro Akküçük, Zeynep 2-305 Carlson, Anders Altan, Hasim 1-137 Castro e Costa, Eduardo Andersen, Marilyne 1-147 Celani, Gabriela Androutsopoulou, Eirini 1-275 Cerovic, Milutin Angeloni, Guilherme 1-157 Chang, Jia-Rey Araneda, Claudio 2-355 Charlton, James Araya, Sergio 1-575 Chatzikonstantinou, loannis Arrobas, Pedro 1-291 Ciftcioglu, Ozer Attia, Shady 1-21, 1-147 Cohen, Itai Avantaggiato, Luigi 2-495 Coimbra, Eugénio Avincola, Eolo 2-29 Colakoglu, Birgul В Côté, Samantha Baharlou, Ehsan 2-165 Coutinho, Filipe Cutellic, Pierre Balakrishnan, Bimal 1-101 Barczik, Günter 2-571 D Barros, Pedro 2-715 Davila Delgado, Juan Manuel Baur, Marco 2-237 de Boissieu, Aurélie Bavraktar, Mehmet Emin 1-375 De Meyer, Ronald Becerra Santacruz, Habid 1-137 De Somer, Pauline Becker, Mirco 1-643 Díaz, César Beirão, José 1-291, 2-705, 2-715 Dieckmann, Andreas Ben Rajeb, Samia 2-605 Di Mascio, Danilo Bereuter, Martin 1-605 Dolas, Caner Bernal, Marcelo 2-595 Donath, Dirk Bernhard, Mathias 1-597 Dritsas, Stylianos Bhagra, Saurabh 1-625 Duarte, José Pinto Bielik, Martin 1-109 Biloria, Nimish 1-529, 2-117 Duddumpudi, Krishna Bittermann, Michael S. 2-335, 2-345 Duro-Royo, Jorge Boevkens, Stefan 2-505 D'Uva, Domenico Bosi, Felipe 1-383 1-337 Both, Katherine E Bourdakis, Vassilis 1-185 Ebertshäuser, Sebastian Boyd, Jeffrey E. 1-467 Economou, Athanassios Brakke, Aaron 1-117 El Ahmar, Salma Bristogianni, Telesilla 2-49 Eloy, Sara Brito, Thiago Mello 1-157 Erdine, Elif Brown, Andre 2-697 Etman, Omar Bühler, Katja 2-279 Ezzeldin, Sherif

1-283

1-375

2-227

1-449

1-69

2-635

2-705

1-633

1-529

1-205

2-137

1-175

2-677

2-273

2-397

2-655

1-393

2-155

2-563

2-627

2-505

1-117

2-485

2-435

2-485

1-655

1-507

1-585

2-315

2-525

2-617

1-539

2-621

1-559

1-459

1-459

1-109, 1-487

2-705, 2-715

2-635, 2-655, 2-687,

2-335, 2-345

F		In, Jessica	1-665
Falcão, Ana Paula	1-265		
Ferreira, Victor	1-439, 2-445, 2-655	J	
Figueiredo, Bruno	2-687	Jabi, Wassim	2-217
Fioravanti, Antonio	1-81, 1-539, 2-29, 2-385,	Jakubal, Vladimir	1-213
	2-495	Janssen, Patrick	2-205
Fiorito, Stefano	1-439	Janusz, Jan	1-91
Florián, Miloš	1-51	Junk, Stefan	2-397
Foged, Isak Worre	2-99	K	
Folcher, Viviane	2-605	R Kaftan Martin	1 600
Fraguada, Luis	1-433	Kallan, Martin	1 105
Fricker Pia	2-545	Kalaouzis, Giorgos	1-185
Fukuda Tomohiro	1-219	Kalay, Yenuda E.	2-59
	1219	Kalvo, Raul	1-655
G		Kanasaki, Kenji	1-/11
Gadelhak, Mahmoud	2-261	Kayser, Markus	1-585
Gallas, Mohamed-Anis	2-107	Kepczynska-Walczak, Anetta	2-453
Gargaro, Silvia	1-81	Kimpian, Judit	2-79
Geddert, Florian	1-109	Kiviniemi, Arto	2-465
Georgakopoulou, Sofia	1-255	Kınayoğlu, Gökhan	2-297
Gerber, David	1-69. 2-175	Klein, Ralf	2-505
Girot Christophe	1-433 2-545	Klofutar Hergeršič, Ana	1-227
Gokmen Sabri	1-497	Knight, Michael	2-697
Gonzalez Uribe Carlos David	1-585	Knippers, Jan	1-549, 2-237
Grast Thomas	2-617	Kocaturk, Tuba	2-465
Greenberg Dan	1-569 2-147	Koch, Volker	2-587
Grochal Barbara	2_217	Koenig, Reinhard	2-195
Guéna François	2_217	Koltsova, Anastasia	2-375
Gün Onur Vüce	2-505 1_61	Kos, Jose Ripper	1-157
Gürel Niban	2 415	Koutamanis, Alexander	2-475
Gulei, Millall	2-415	Kretzer, Manuel	1-615
н		Krüger, Mário	2-655, 2-687
Haeusler, M. Hank	1-233	Kucukoglu, J. Gozde	2-273
Halin, Gilles	2-107	Kunze, Antie	1-41
Hanafi, Mohamed	1-539	Kurilla, Lukáš	1-51, 2-555
Hanna, Sean	2-39		
Hanzl, Małgorzata	1-319	L	
Havmaker, John	2-595	LaMagna, Riccardo	1-549
Heinzelmann Florian	1-175 2-49	Laucks, Jared	1-585
Heitor Teresa	1-337 1-403	Leclercq, Pierre	2-605
Hesselaren Lars	2-39	Lecourtois, Caroline	2-563
Hirschberg Urs	1-683	Li, Di	2-697
Hofmeyer Herm	2-155	Lin, Jui-Yen	2-21
Hong Soung Wan	2-50	Lin, Shih-Hsin Eve	2-175
Hong Sung Min	2-39	Loffreda, Gianluigi	2-495
Hulin Jaroday	2 / 2 2_255	Lorenz, Wolfgang E.	2-667
nuilli, Jatoslav	2-233	Lotte, Fabien	1-393
1		Lückert, Angelika	2-587
lanni, Manuela	1-31	· 2	
Igarashi, Takeo	1-693		
-			

#### м

Makris, Michael	1-69
Malheiros, Victor	1-383
Margotto, Mário	1-383
Marques, Rui	2-621
Martens, Bob	2-279
Massara, Bruno	1-383
Matějovská, Dana	1-213
Mateus, Luís	2-445, 2-655
Medeiros, Valério	1-337
Melsom, James	1-433
Mendes, Leticia Teixeira	2-705
Menges, Achim	1-549, 2-165, 2-237
Miltiadis, Constantinos	1-517
Mitani, Jun	1-693
Mohammed-Amin, Rozhen K.	1-467
Moleta, Tane	1-507
Moloney, Jules	1-507
Morales Beltran, Mauricio	2-117
Mostafavi, Sina	2-117
Moya, Rafael	2-69
Mueller, Volker	2-39, 2-185
Mumovic, Dejan	2-79
Munkel, Georg	2-545

#### Ν

Narahara, Taro	1-673
Nicknam, Mahsa	2-595
Nielsen, Stig Anton	1-413
Noble, Doug	1-69
Nourian, Pirouz	1-357
Nováková, Kateřina	1-213, 2-555
Novembri, Gabriele	2-29
Nunes, Mário	1-403

#### 0

1-693
2-289
1-625
1-101
1-167, 2-415
1-439
1-585
1-127
1-195, 2-305
1-423
2-475

1-185

Papasarantou, Chrissa

Parascho, Stefana	2-237
Parisel, Claude	2-325
Paterson, Greig	2-79
Patlakas, Panagiotis	1-137
Pavlicek, Jiri	2-255
Pla-Catala, Anna	2-579
Pungerčar, Enej	1-227
R	
Reichert Steffen	1-549
Pezvani Samaneh	1_357
Pichardson Adam	2-217
Roccasalva Giusoppo	2-217 1_41
Polando Andrea	1-41 2_315
Roman Miro	2-315
Romão Luíc	2-403
Romado, Luis Povo Ana Filina	2-077
Ruz, Holona	1 265
Rud, Helefid	1 642
Rumpi, Montz	1-043
Russell, Peter	2-403
S	
Saey, Rik	2-505
Salim, Flora	2-69
Sánchez de León, Michelle	1-31
Sariyildiz, Sevil	1-357, 2-137
Schaffranek, Richard	1-347
Schaumann, Davide	2-59
Schindler, Christoph	1-605
Schloz, Manuel	1-549
Schmitt, Gerhard	1-41, 1-255, 2-195, 2-375
Schneider, Sven	1-109, 1-487
Schwartz, Mathew	2-365
Schwinn, Tobias	1-549
Semlali, Anis	2-325
Serdoura, Francisco Manuel	1-439
Sevtsuk, Andres	1-655
Shah, Mahnaz	1-329
Sharaidin, Kamil	2-69
Simeone, Davide	2-59
Sokmenoglu, Ahu	1-301
Sonmez, N. Onur	1-301
Stavrakantonaki, Marina	2-535
Steinø, Nicolai	1-195
Stojanovic, Djordje	1-633
Stoutjesdijk, Pieter	1-719
Strobbe, Tiemen	2-185, 2-627
Sun, Yimin	2-645
Su, Ping	2-645
Symeonidou, Ioanna	1-683

т		Vrouwe, Ivo	1-703
Tabatabai, Ali	1-605	14/	
Taguchi, Masaharu	1-219	Waimar Frédéric	1 540
Takenaka, Tsukasa	2-289	Warnelink LW E (Lane)	1-549
Tamke, Martin	1-605	Wang Dig Llung	2-4/5
Tanaka, Hiroya	1-693, 1-711	Waigala Jakah	2-21
Tapias Pedraza, Estefania	1-41	Welgele, Jakob	1-549
Tenpierik, Martin	2-137	Wester Mark	1-1/5
Teuffel, Patrick	2-49	Weston, Mark	1-309, 2-147
Thompson, Emine Mine	1-205	Williams Mani	2-39
Tidafi, Temy	2-325	Wurzer Cabriel	2-09
Tolba, Osama	1-459	Wurzer, Gabrier	2-219
Tomé, Ana	1-403	Х	
Tompson, Tim	1-233	Xiong, Lu	2-645, 2-725
Trento, Armando	2-385	Xiong, Wei	2-725
Treyer, Lukas	2-195	5,	
Tunçer, Bige	2-375	Y	
Turrin, Michela	1-175, 2-137	Yazar, Tuğrul	2-247
V		Yazici, Sevil	2-127
Van Camponhout Jan	2 627	Yıldırım, Miray Baş	1-195
van Campennout, Jan	2-027	Yoshida, Hironori	1-665
Vardauli Theodora	1 242	7	
Vasku Michael	1-245	– Zajíčková Veronika	2-515
Velasco Bodrigo	1_117	Zarzycki Andrzej	2-425
Veliz Felipe	1-575	Zhang Hongxia	2-725
Verbeke Johan	1-423	Zolotovsky Ekaterina	1-575
Vidmar Jernei	1-311	Zreik Khaldoun	2-605
von Both Petra	2-525 2-587	Zünd, Daniel	1-255
von Mammen, Sebastian	1-467	Zupančič, Tadeja	1-227

# **Computation and Performance**

# Volume 2

This is the second volume of the conference proceedings of the 31st eCAADe conference, held from 18–20 September 2013 at the Faculty of Architecture, Delft University of Technology, Delft, The Netherlands.

The theme of this conference is the role of computation in the consideration of performance in planning and design.

Since long, a building no longer simply serves to shelter human activity from the natural environment. It must not just defy natural forces, carry its own weight, its occupants and their possessions, it should also functionally facilitate its occupants' activities, be esthetically pleasing, be economical in building and maintenance costs, provide temperature, humidity, lighting and acoustical comfort, be sustainable with respect to material, energy and other resources, and so forth. Considering all these performance aspects in building design is far from straightforward and their integration into the design process further increases complexity, interdisciplinarity and the need for computational support.

One of the roles of computation in planning and design is the measurement and prediction of the performances of buildings and cities, where performance denotes the ability of this built environment to meet various technical and non-technical requirements (physical as well as psychological) placed upon them by owners, users and society at large.

eCAADe — the association for Education and research in Computer Aided Architectural Design in Europe — is a non-profit making association of institutions and individuals with a common interest in promoting good practice and sharing information in relation to the use of computers in research and education in architecture and related professions. eCAADe was founded in 1983.

All papers of these proceedings are accessible via CumInCAD (cumincad.scix.net).





ISBN: 978-94-91207-05-1